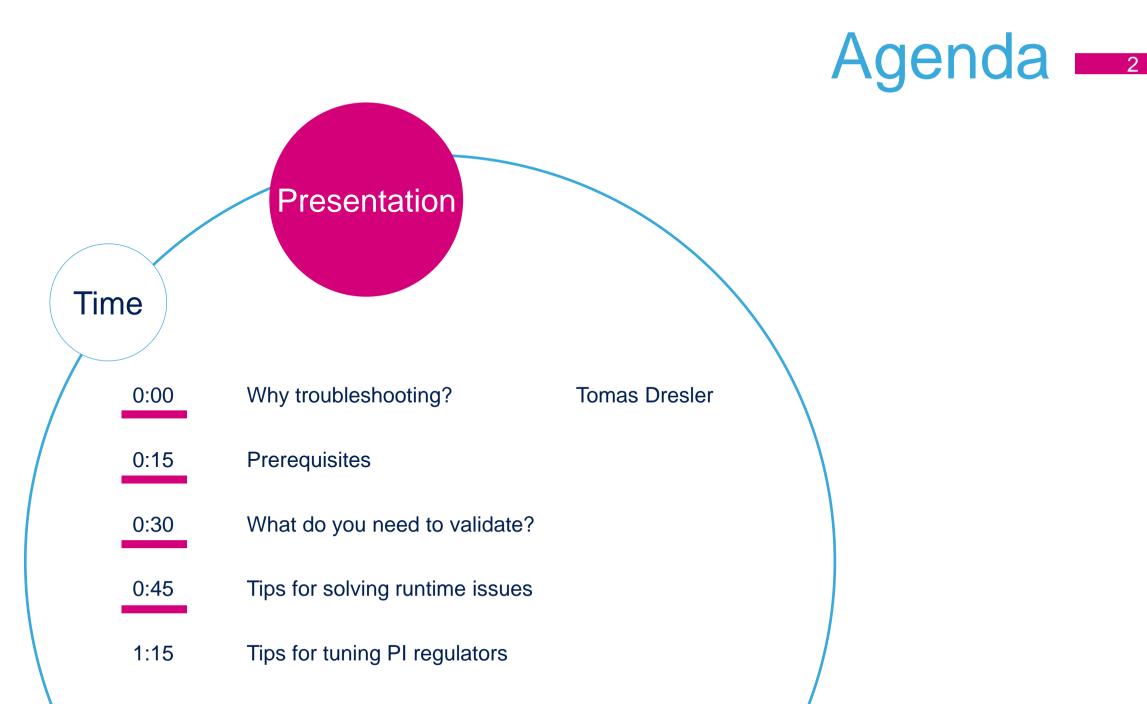
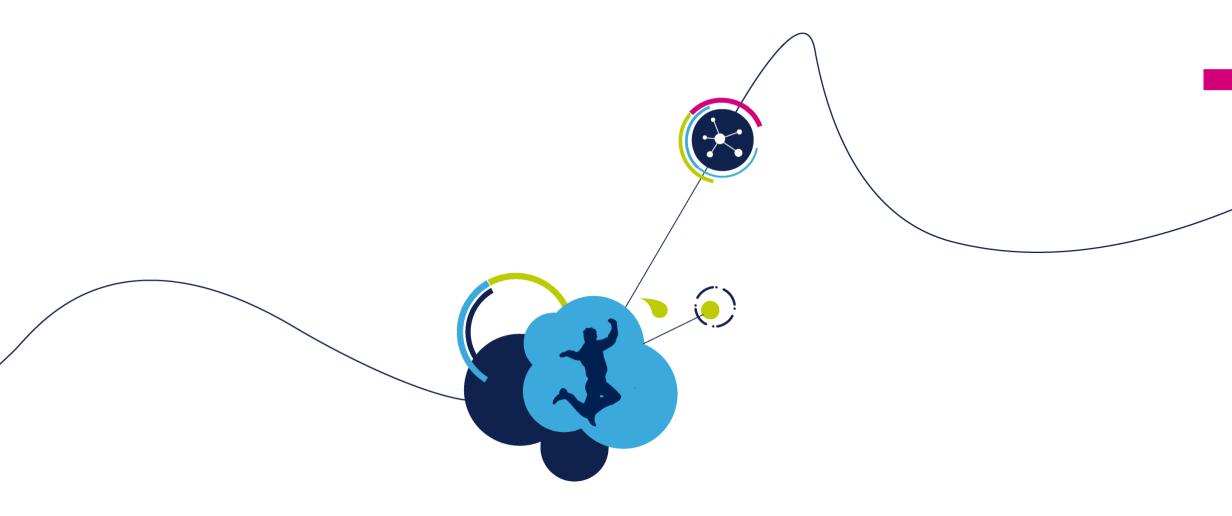
Troubleshooting of your BLDC motor

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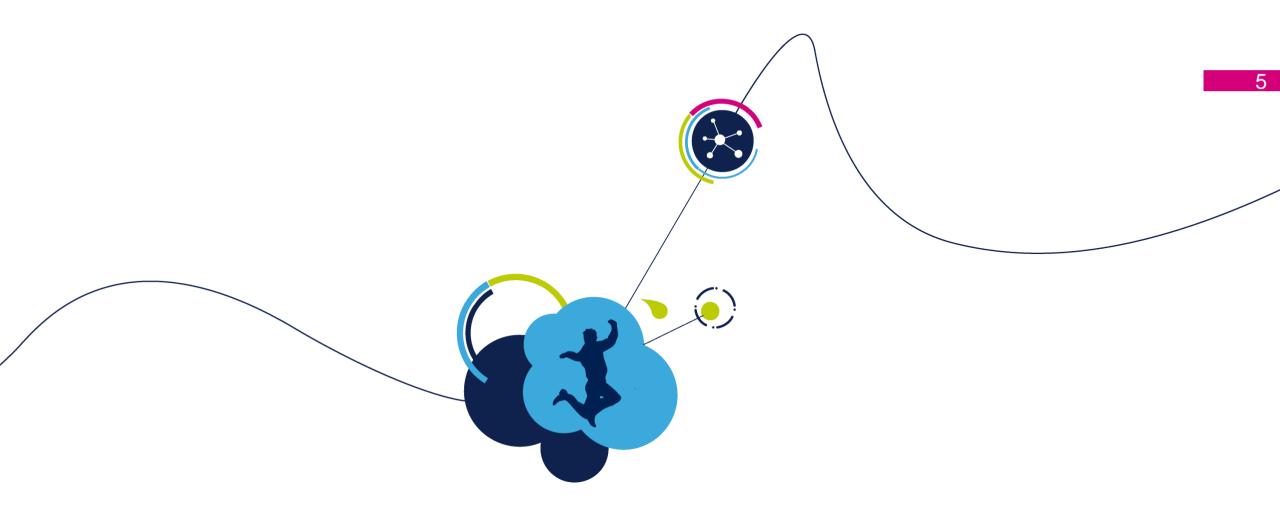
Why troubleshooting?



Why troubleshooting?

- Each motor application is different:
 - Load, changing over time
 - Electrical parameters differ from application to application
 - The assumptions in the SDK target mainstream engines, not special ones
 - i.e., very low inductance windings (high-speed motors)
 - Very high load variations (no-load vs. heavy load on the clutch)
- Every designer was a beginner
 - And made some assumptions that were not right,
 - Or omitted some crucial detail,
 - Or reused old design without checking the setup too much etc.





Prerequisites



Prerequisites

- What do I need to successfully debug my motor application?
 - Multichannel Digital Signal Oscilloscope
 - with current probe
 - and several (high)-voltage probes
 - Insulation transformer(s) (for high-voltage applications)
 - Multimeter
- What else?
 - Board schematics
 - DAC outputs
 - Debugger (possibly insulated)
 - Serial to USB cable (possibly insulated)



Prerequsites 7

DAC outputs

- Display up to 2 run-time values of variables used in the FOC algorithm using oscilloscope
- Allow immediate look at internal processes
- I_{alpha}, I_{beta} show quality of current reading if noisy or distorted, validate current reading path and setup t_{noise}, t_{raise} according to FOC SDK User Manual
- b-emf_{alpha}, b-emf_{beta}, observed el. angle if noisy or unstable, G2 is too high or measurement of R, L, K_e of your motor are wrong (within range of tens of %)
- Options for DAC output supported by MC FOC SDK:

DAC	PWM	SPI
Must be supported by	Needs RC filter	Requires external
MCU and your HW	Cheap, output has	DAC
Very precise	exponential delay	Very precise





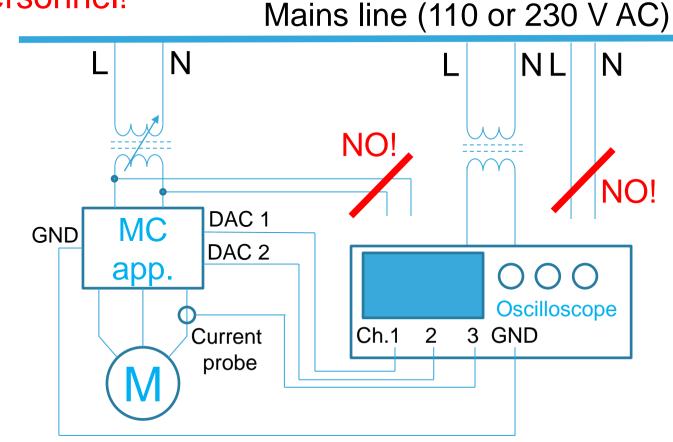
- UART (via USB) connection allows natively
 - debugging with MC Workbench in Monitor mode,
 - changing runtime parameters (coefficients of many PI regulators, G2, required speed or torque etc.),
 - observing speed and tuning PI coefficients of speed regulator in runtime



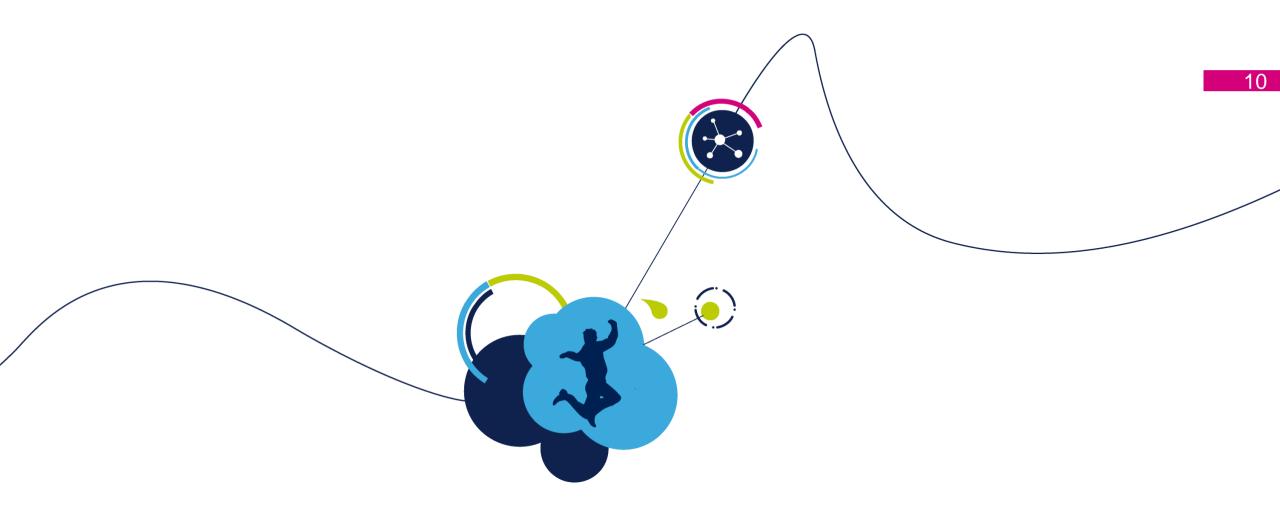


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- Insulation transformer(s), oscilloscope usage in high-voltage systems
- Operate only by certified personnel!
 - Reduce risk of equipment damage
 - Reduce risk of injury or death
 - Only for mains (AC) rated applications







What do you need to validate?



Validation

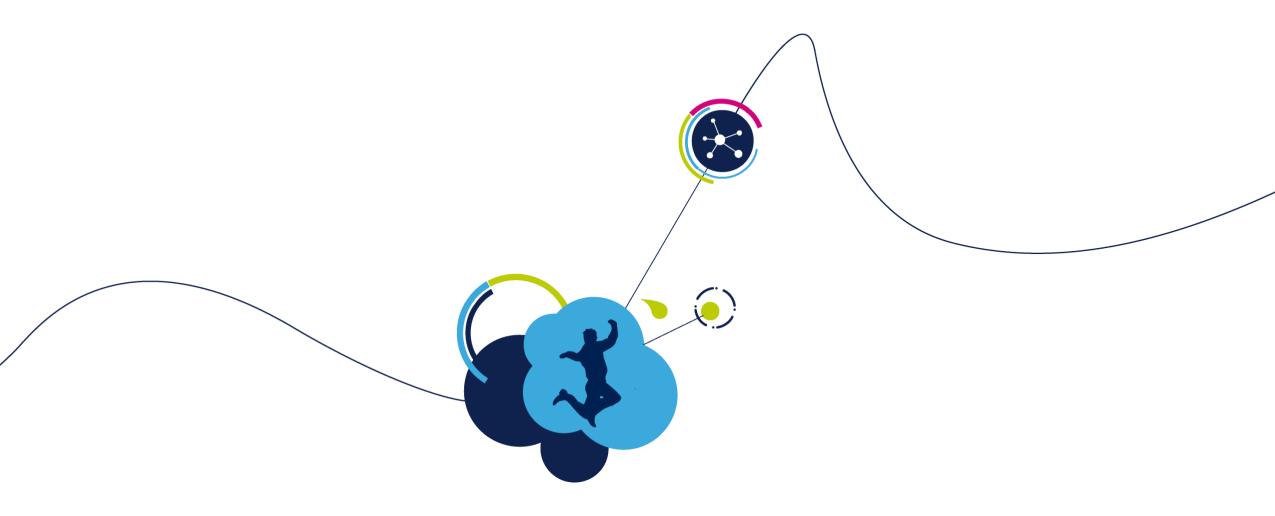
- Before I switch the application on
 - Proper jumper setup and soldering switch configuration for:
 - Current reading topology (1-shunt, 3-shunt)
 - Speed sensor configuration (Hall, encoder, its derived supply: 5V/3.3V)
 - Overcurrent, over-temperature reaction mechanism
 - Polarity and rating of supply voltage, setup and range of DC-DC converter
 - Is isolation needed between mains and your application and your oscilloscope?
 - Does my power supply have current limiting option? Initially set to small value (tens of mA)!
 - Are my DAC outputs connected to oscilloscope?



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- After I switch the application on
 - Is the supply current within a reasonable limit?
 Without motor running, only few tens of mA are suggested.
 Only after this check, set current limitation to operating limit!
 - Is your application alive and communicating (via UI, USART etc.)?
 - When I start the motor, is the overcurrent reported by power supply or by overcurrent mechanism of the power stage?
 - Do I see the currents reported by DAC outputs on my oscilloscope when my motor runs?







- Initial application engineer's decision tree:
 - 1. If it burns, check HW
 - 2. If it doesn't move, check power stage setup (PWM, ADC, OC)
 - 3. If it moves a little, check alignment, start-up and rev-up
 - 4. If it moves, but fails at speed change, check G2 and Speed PI regulator
 - 5. If it moves, but speed is unstable, check Speed PI regulator
 - 6. If it moves well, you're finished! Congratulations!
- Application design
 - 1. Does it need speed control? Use torque mode!
 - 2. Does it really need speed control? Use speed mode, but tune Speed PI well!



- I don't see changes of my SW in the application
 - Did you generate updated header files in correct folder or placed them there?
 - Did you recompile your SW after applying the changes?
 - Did you load new SW to your application?
 - Isn't the debugger the other USB cable connected you your PC?



- Does your application read, evaluate and react on SDK error states?
 - If not, rethink your SW and ask the question again!
- "FOC duration" error shows up, motor doesn't move at all
 - The PWM frequency is too high for CPU to handle FOC algorithm in time
 - Increase "FOC execution rate" by one in Drive settings
 - Revalidate your IRQ priorities MC FOC SDK must always have the highest interrupt priority of all! Your motor depends on it!



- Best PWM frequency?
 - Low enough to reduce switching losses (down to ~8 kHz)
 - High enough to manage low inductance motors (up to ~30 kHz) and above acoustic noise band (human ear can listen up to 22 kHz)
 - CPU load can be reduced by increasing "FOC execution rate"
- Best start-up settings (start with, tune to your application later)
 - Speed ramp duration 3000 ms
 - Speed ramp final value 30% of maximum motor speed
 - Current ramp final value 50% of nominal motor current
 - Include alignment (2000 ms, 50% of nominal motor current)
 - Minimum start-up speed set as 15% of maximum motor speed



- "Over current" detected immediately at start-up
 - Wrong current sensing topology single-shunt instead of three-shunt? Did you check your jumpers?
 - Isn't power stage damaged by overcurrent? Check your MOSFETs for short circuit!
 - Verify and correct current path gain, ADC input, polarity of PWM outputs
 - The current regulation bandwidth is too high in Drive settings, reduce current regulation bandwidth down to 2000 rad/s for 3-shunt and 1000 rad/s for 1-shunt. Maximum value is 9000 rad/s, resp. 4500 rad/s.
 - PWM frequency is too low phase current may rise too quickly esp. in low-inductance motors increase PWM frequency, to avoid "FOC duration" error see previous slide



- "Speed feedback" appears after sudden acceleration or deceleration
 - The runtime uses speed variation for detecting anomalies, thus big speed change over short time can trigger this error
 - Use speed ramps to reduce acceleration
 - Observer gain G2 is too high and speed estimation generates too much noise:
 - Decrease G2 by 2, 4, 6, 8 and retry...
 - Detect by displaying b-emf alpha and beta on the DACs they shall be sinusoidal. Too much noise or distortion means too high G2 estimation
 - Test in torque mode. If this mode runs stable, speed PI regulator needs re-tuning
 - Too low variance threshold. Increase gradually up to 100% or increase speed FIFO depth (as power of 2).
 Beware, this parameter significantly reduces sensitivity for rotor locked condition detection!



"Speed feedback" appears immediately after start-up

- Start-up validity can be detected too early. Return to Start-up parameters and increase # of successful consecutive start-up tests (not more than 4-5) and minimum start-up speed to 15% of maximum motor speed
- Use Rev-up algorithm to align gradually forced torque ramp with sensor-less control algorithm output – this avoids sudden speed change at the transition between open loop and closed loop
- "Start-up failure" appears after motor initially moves, but stops before **Rev-up**
 - The torque (current) at higher start-up speed is insufficient to accelerate to validation speed
 - Decrease acceleration rate set speed ramp final value to 30% of motor max. speed



- Increase start-up current from ~50% up to 100% of nominal current
- Enable alignment phase for more deterministic start-up or use advanced start-up

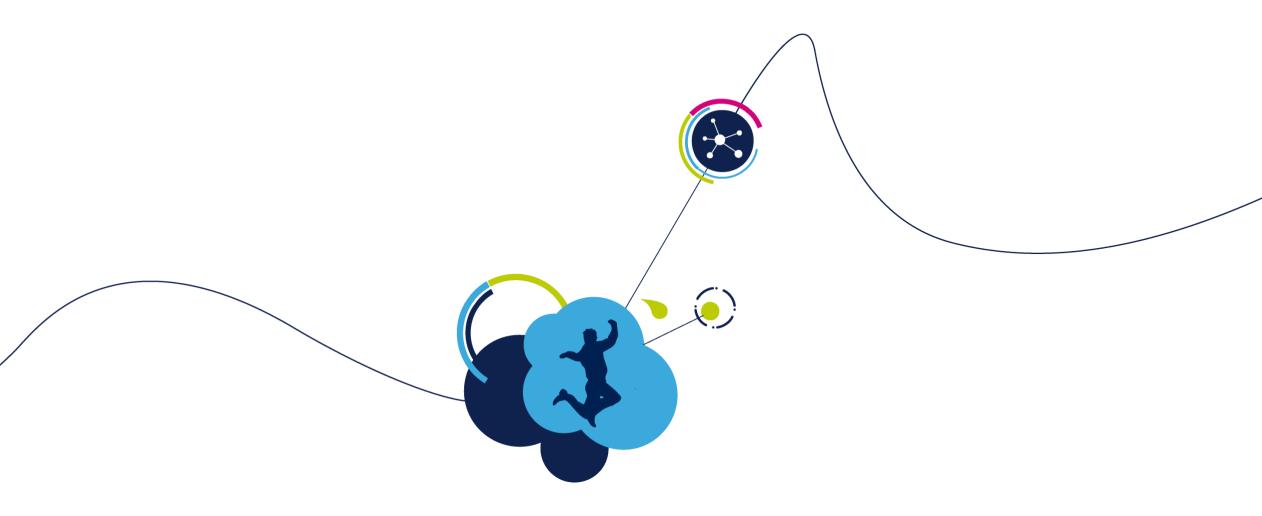
- My motor doesn't start immediately
 - You have opted for alignment motor waits for stabilization in specific position
 - "On-the-fly start-up" has been selected detection phase has started and waits some time for rotation signal – if none is found, standard alignment and start-up applies



• Speed or control is unstable below 5% of maximal motor speed

- The sensorless algorithm is stable down to 5-7% of maximum speed. Below that speed the noise from current reading is too high for proper rotor position estimation.
- Solution is twofold:
 - 1. Use Hall sensors for low speed region and sensorless at medium-to-high speeds
 - 2. Use HFI sensorless algorithm (only available for anisotropic motors and MCUs with FPU)
- Speed control is unstable at various speeds
 - Load changes in non-linear fashion
 - May be too light at low and high speeds (i.e. air pump) and heavy at medium speeds
 - May require different Speed PI tuning at different speeds with linear interpolation between the regions



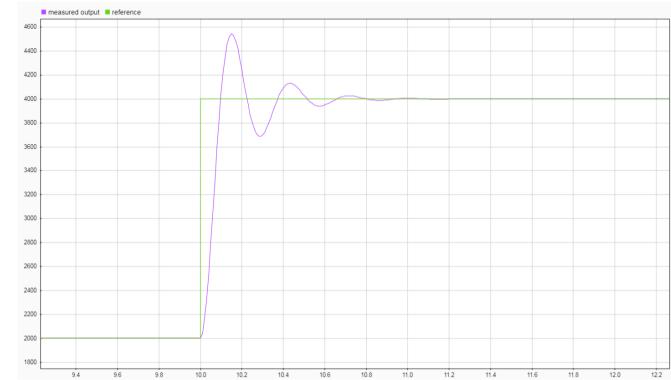




- There are many PI(D) regulators in the SDK:
 - I_q, I_d current regulators within FOC model
 - PLL PI in the position/speed reconstruction block
 - Flux weakening PI regulator
 - Speed PI regulator
- Most of them are tuned by Workbench, but response of some of them depends on the physical application around the SW model, i.e.
 - Speed PI depends on the load inertia
 - I_q, I_d current regulators depend on power stage, inductance, PWM frequency



- There exist many methods for proper tuning, let's start with manual
- The tuning requires a step change in the required quantity (speed, load, current) and measurement of the regulated quantity response
- An example is change of the required speed as a step from 2000 RPM to 4000 RPM. The response is the real speed over time:

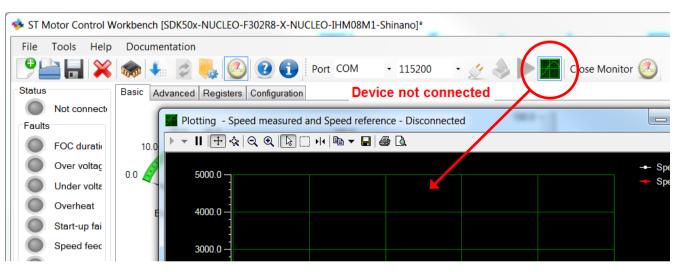


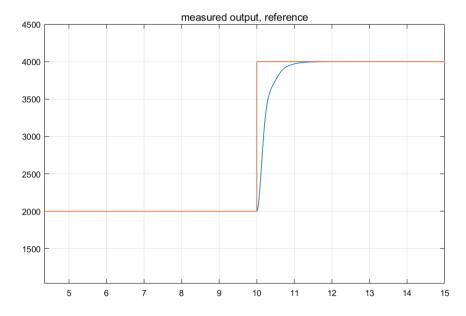


- On previous slide, we saw damped oscillation response this may be unwanted behavior, so let's mention some rules of thumb!
- If there is an overshoot, change the ratio K_p/K_i to avoid it or vice versa
- If the shape is exponentially closing to the required value, keep the ratio K_p/K_i, but proportionally change both K_p and K_i to increase or decrease the slope.
- Try this at different speeds and loads and choose conservative estimation – avoid undamped oscillation at all costs!



- Such chart can be displayed in MC workbench, Monitor mode, via Plotter window
- Otherwise use DACs and oscilloscope
- Optimum reaction, if overshot is undesired, is on the following picture:



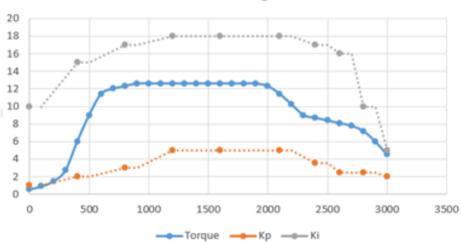


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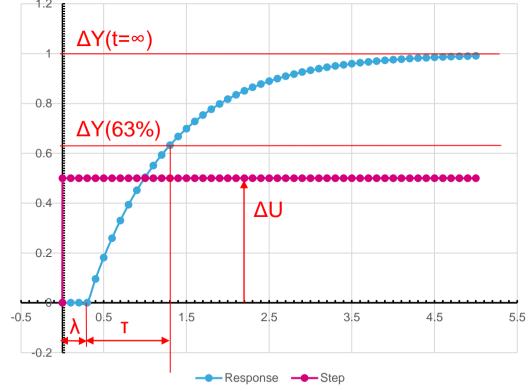
 If the load torque changes with speed, different tuning may be needed at different speeds. An example of optimal value of K_p, K_i vs. speed is on the following picture:



 Such K_p, K_i interpolation may need to be implemented in user SW for the Speed PI



- Another more analytical methods need some measurements in the torque mode:
 - Determine stabilized speed response Y(t=∞) on torque step U:
 - Determine Process dead time (λ)
 - Determine Time constant (T) when speed crosses 63% of the speed step (between stabilized value and initial speed)
 - Read PI process frequency f_s (usually 2 kHz)



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- Typically the motor with connected load is a first order system (with simple exponential response) with process delay λ
- In such case, simple calculation is needed:
 - Process gain

$$K = \frac{\Delta Y(t=\infty)}{\Delta U}$$

- Here the ΔY has unit of dpp (digits per PWM) and ΔU is change in Compare register of MC timer
- Let's consider PI(D) regulator of this form:

$$y(s) = K_p \left(1 + \frac{1}{T_i \cdot s} + T_d \cdot s \right) e(s)$$



• Ziegler-Nichols method (overshoot, aggressive)

Туре	K _p	Τ _i	т _d
Р	$\frac{1}{K}\frac{\tau}{\lambda}$	∞	0
PI	$\frac{0.9}{K}\frac{\tau}{\lambda}$	3.33 · λ	0
PID	$\frac{1.2}{K}\frac{\tau}{\lambda}$	$2.0\cdot\lambda$	$0.5 \cdot \lambda$



Cohen-Coon method (moderate to conservative)

Туре	К _р	Τ _i	Τ _d
Ρ	$\frac{1}{K}\frac{\tau}{\lambda}\left(1+\frac{1}{3}\frac{\lambda}{\tau}\right)$	∞	0
PI	$\frac{1}{K}\frac{\tau}{\lambda}\left(0.9 + \frac{1}{12}\frac{\lambda}{\tau}\right)$	$\lambda \left(\frac{30 + 3\frac{\lambda}{\tau}}{9 + 20\frac{\lambda}{\tau}} \right)$	0
PID	$\frac{1}{K}\frac{\tau}{\lambda}\left(\frac{4}{3} + \frac{1}{4}\frac{\lambda}{\tau}\right)$	$\lambda \left(\frac{32 + 6\frac{\lambda}{\tau}}{13 + 8\frac{\lambda}{\tau}} \right)$	$\lambda \left(\frac{4}{11 + 2\frac{\lambda}{\tau}} \right)$



Conversion to discrete PI(D) regulator with sampling frequency f_s

$$K'_{p} = K_{p}$$
$$K'_{i} = \frac{K_{p}}{\tau_{i}} \frac{1}{f_{s}}$$
$$K'_{d} = K_{p}\tau_{d}f_{s}$$

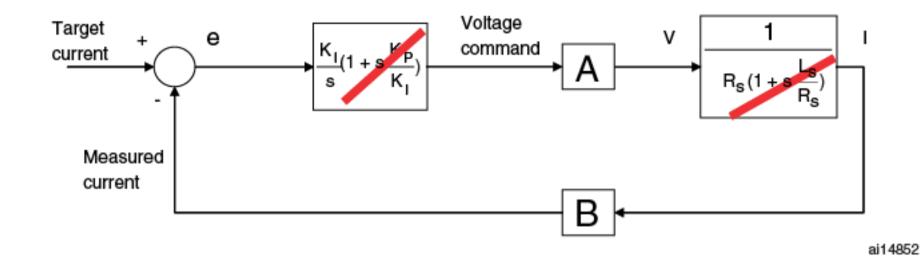
• Calculated values shall be expressed as ratios $\frac{K'_x}{2^N}$ and put in MC workbench, K'_x being in 16-bit range (±32767)



- After calculating the PI coefficients, one still needs to tune them manually
- These equations are valid in the range $0.1 < \frac{\lambda}{\tau} < 1,$ otherwise other type of tuning is needed



- Another method works in time domain with a priori knowledge of motor and load inertia (~L_s) a mechanical resistance (~R_s)
- By substituting K_P/K_I with L_S/R_S ratio, one can perform pole-zero cancellation as shown below, calculating K_P as on previous slide:





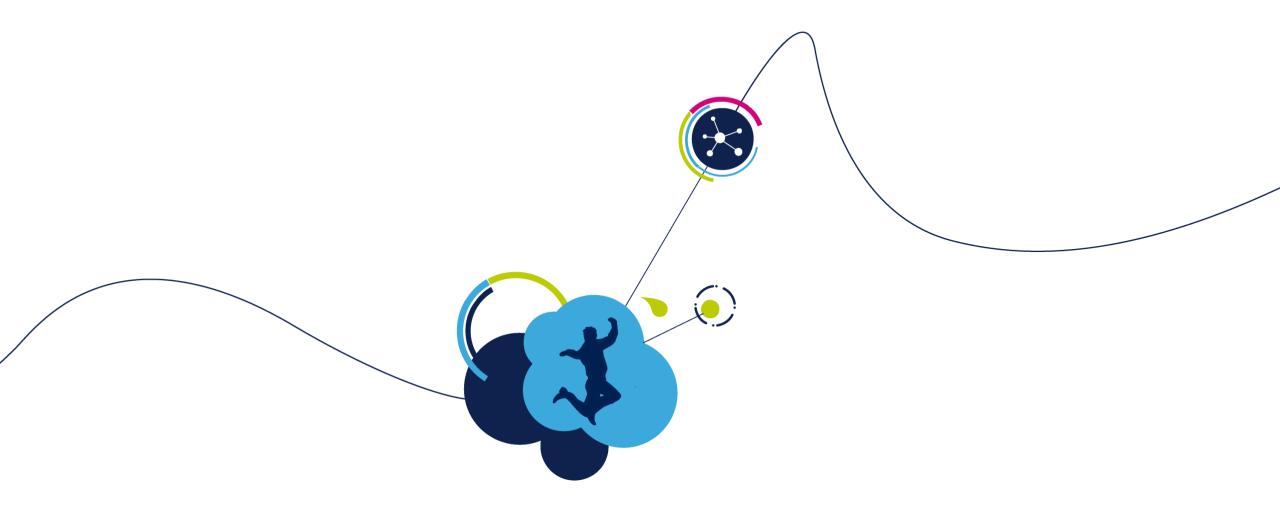
- In case of second-order and more complex or interlinked systems (combined exponential behavior), the response measurement and calculation are complex and discussed in control theory literature, i.e. zero-pole mapping regulators
- Such example shall use PID regulator with derivative component or even more complex (polynomial) regulators
- Small filter with τ'=0.1τ for the error component may be introduced before PI(D) regulator, too



Used literature:

- http://educypedia.karadimov.info/library/pidtune2.pdf
- http://www.kirp.chtf.stuba.sk/moodle/pluginfile.php/66882/mod_resourc e/content/0/tidsdiskret_pid_reg.pdf
- https://pdfs.semanticscholar.org/116c/e07bcb202562606884c853fd1d1 9169a0b16.pdf
- Matlab: pidtune, pidtool
- https://www.biricha.com





Thank you!

